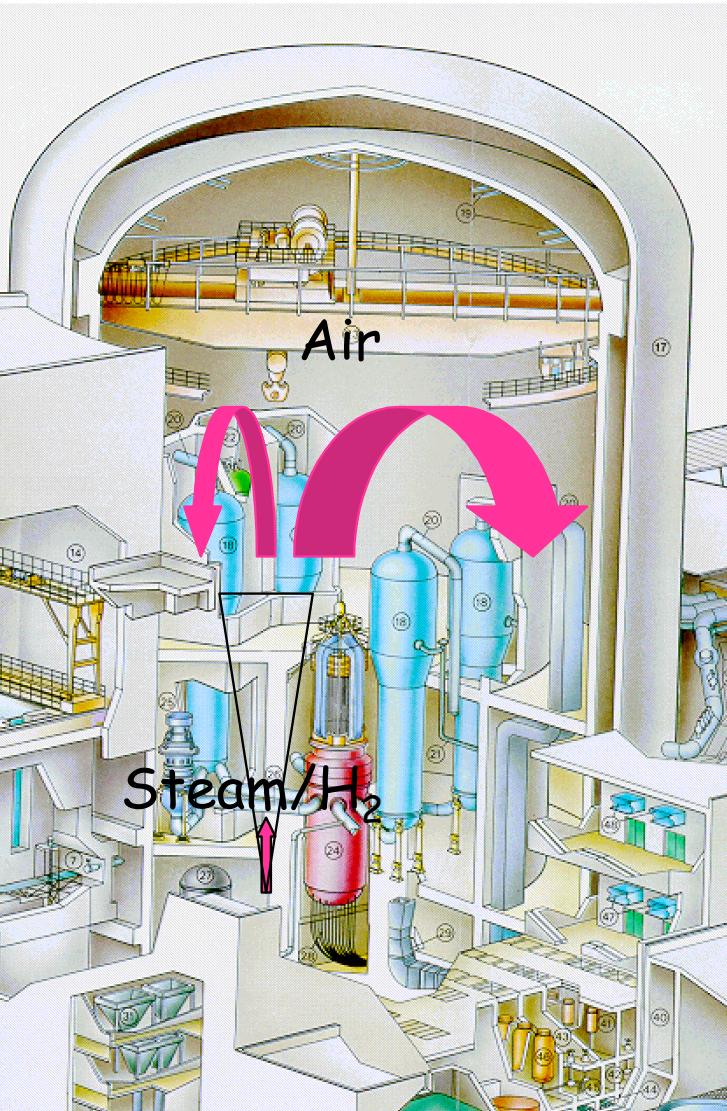


# PAR elevation influence study

*F.Dabbene*

**Club CAST3M 2009**

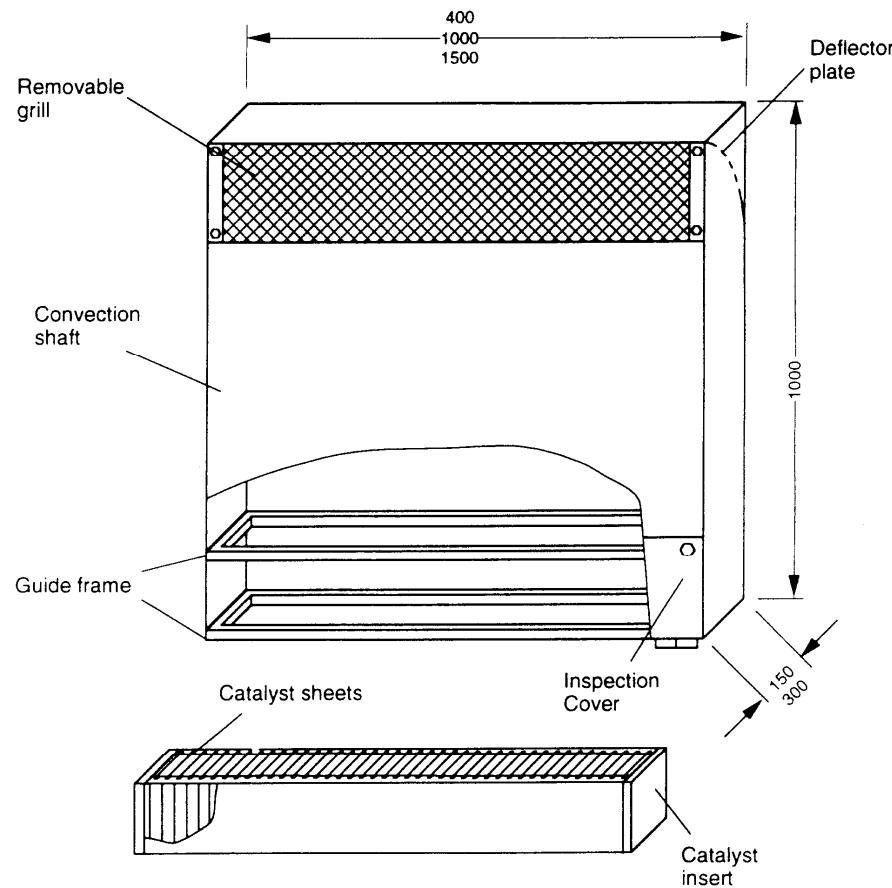
26 novembre 2009 • PARIS, FRANCE



- Containment Thermalhydraulics during severe accident
- Containment initially filled with Air (50 to 80000 m<sup>3</sup>)
- Before core degradation:
  - Hot steam released into the containment (jet/plume)
  - Bulk condensation and wall condensation in presence of non-condensable gases (Air)
  - Natural or mixed convection flows
- Core degradation:
  - Hydrogen (reduction of steam by Zircaloy claddings) released into the containment (with or without steam)
  - H<sub>2</sub> risk

# Principle of Passive Autocatalytic Recombiner (PAR)

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1. Gas enters at the PAR bottom
2. Hydrogen contacts the plates
3. Catalytic reaction begins
4. Reaction heats the gas and the PAR housing
5. Gas rises and leaves at the top of the PAR
6. Natural convection takes place (pumping effect)

# Outline

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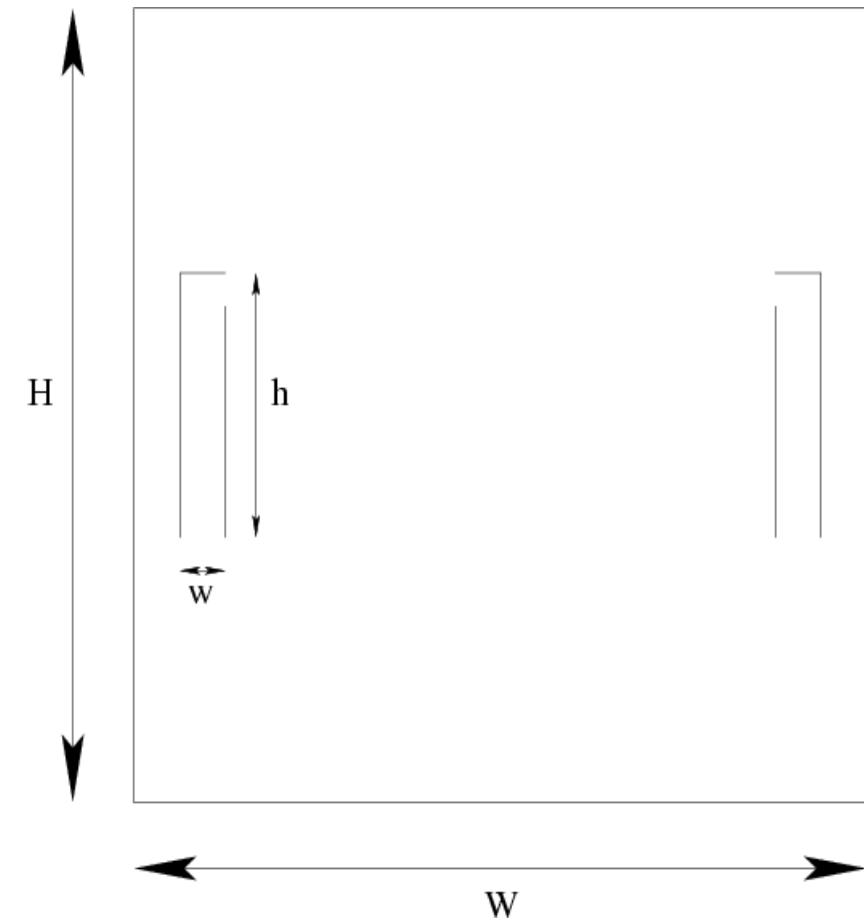


- PARIS benchmark
- Flow structure analysis
- PAR elevation influence

# PARIS benchmark (SARNET, WP12.2)

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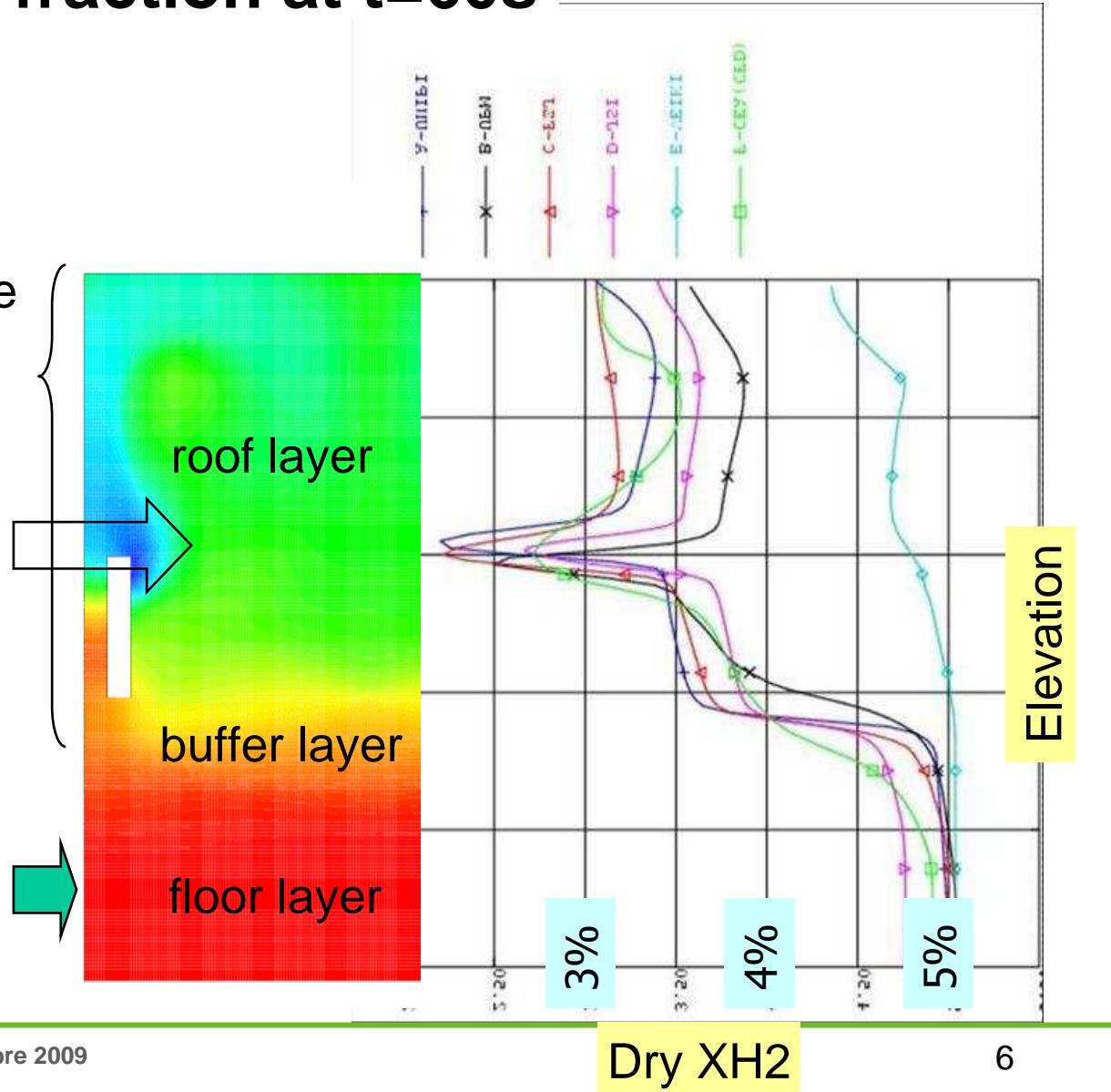
- PAR elevation influence on hydrogen distribution: set the PAR at the half box elevation
- Natural convection loop interaction: one PAR on each side
- PAR is a SIEMENS FR90/1-150 like one ( $h=1\text{m}$ ,  $w=0.2$ , 15 plates)
- SIEMENS H<sub>2</sub> consumption (kg/s) given by  $\min(X_{h2}, X_{o2}, 0.08)(Ap+B)$  with  $A=0.48E-8$  and  $B=0.58E-3$
- Homogeneous initial mixture at 393K, saturated steam, dry  $X_{h2}=5\%$  and air mass the one at 1bar and 298K
- No heat and mass transfer through walls



# Dry H<sub>2</sub> molar fraction at t=60s

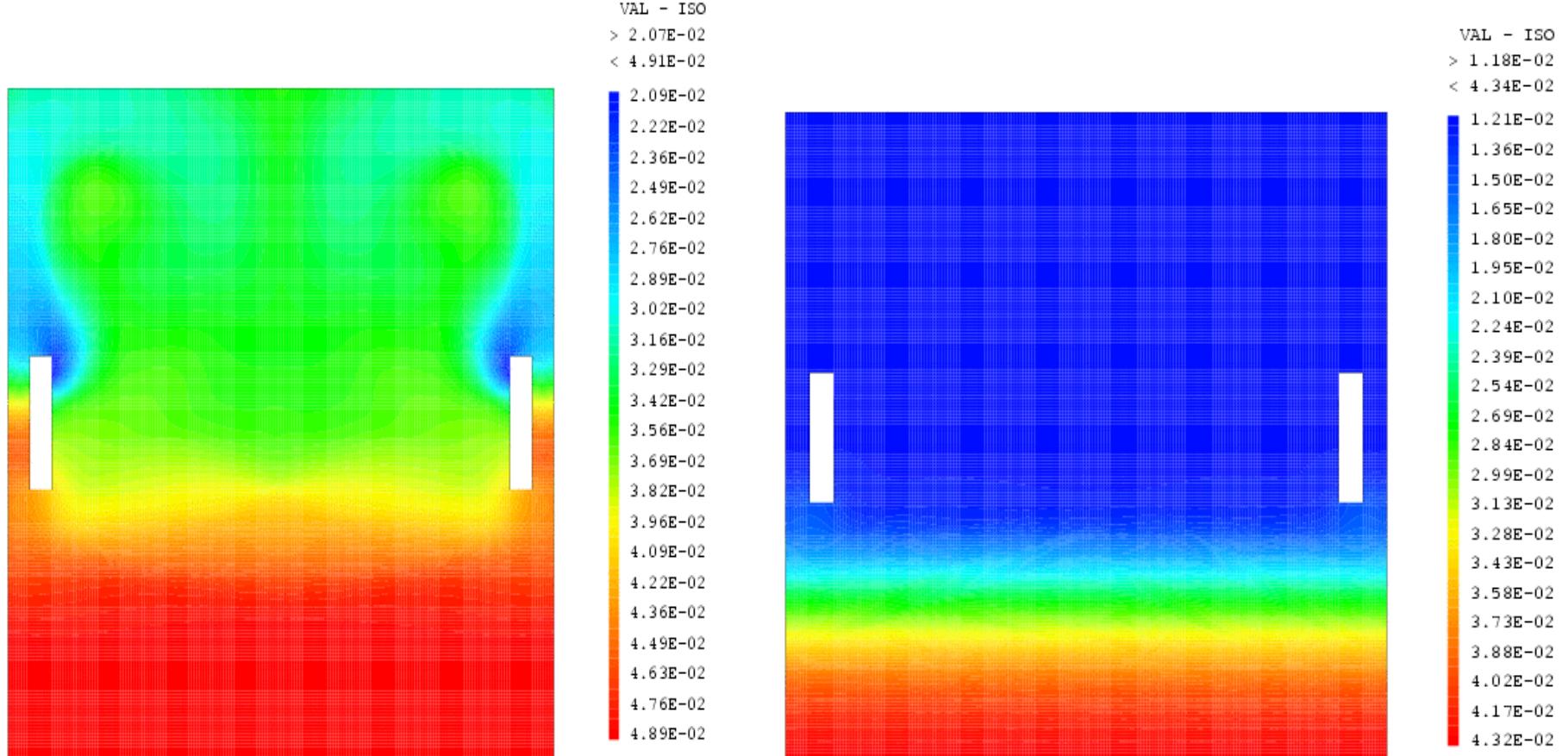
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- Fast H<sub>2</sub> depletion from the ceiling to 0.5m below the PAR (roof layer).
- PAR exit interaction with the atmosphere remains unclear and modify H<sub>2</sub> depletion (inertia and buoyancy balance, turbulence, etc.).
- Stable H<sub>2</sub> stratification in the floor layer due to adiabatic wall boundary conditions.

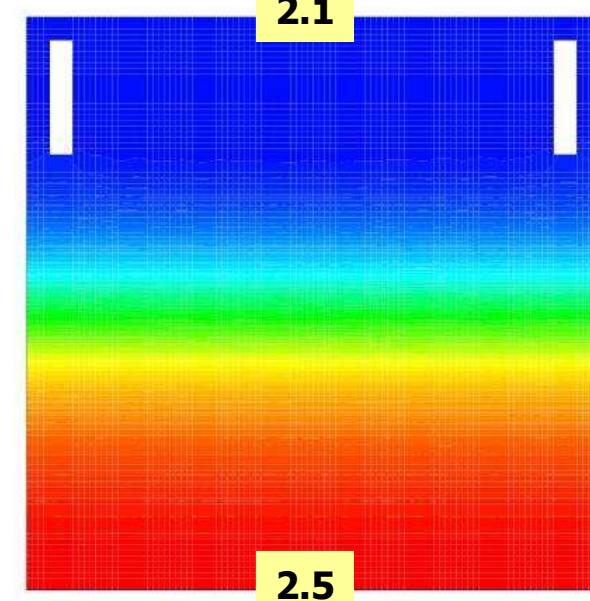
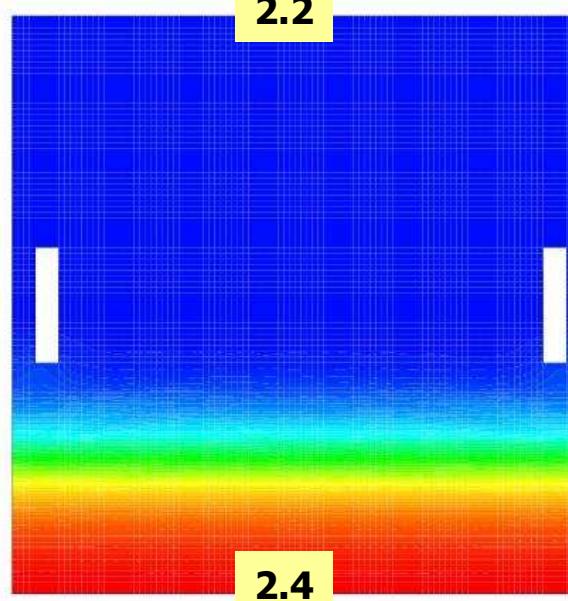
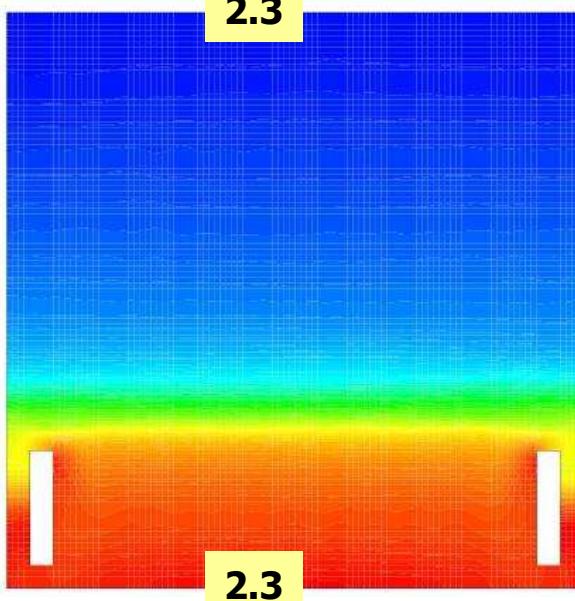
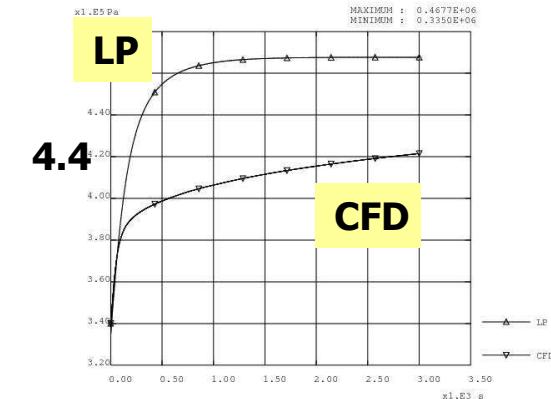
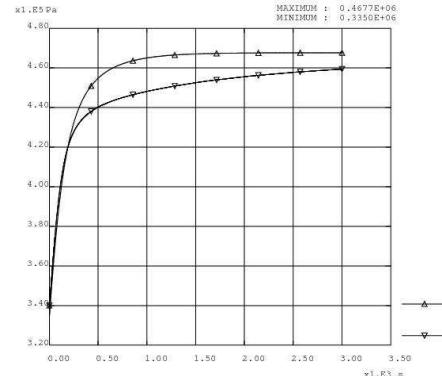
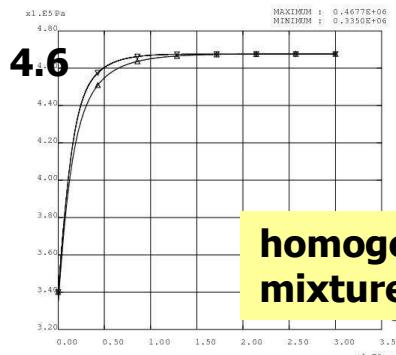


# Dry H<sub>2</sub> molar fraction at t=60s and 600s

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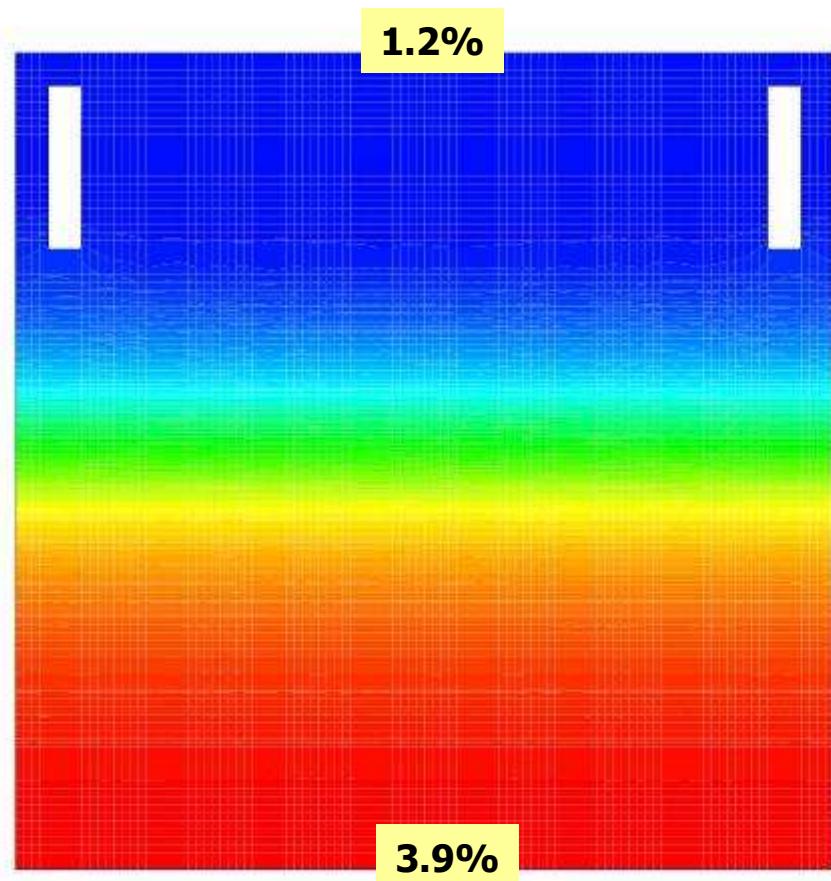
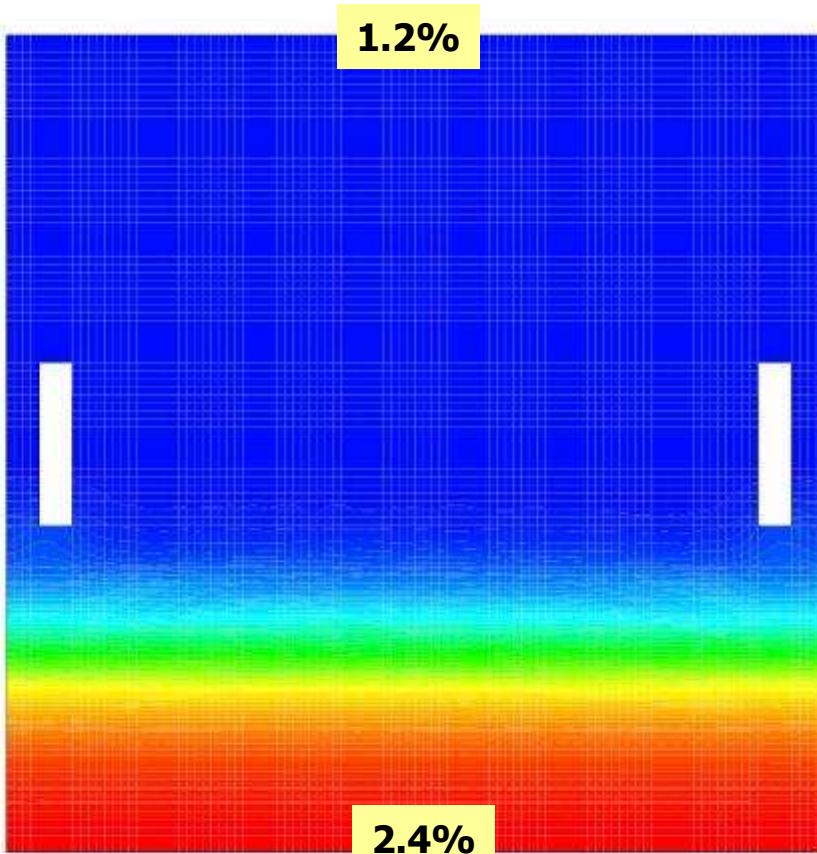
# Pressure evolution and density at t=3000s



## Dry Xh2 at t=3000s

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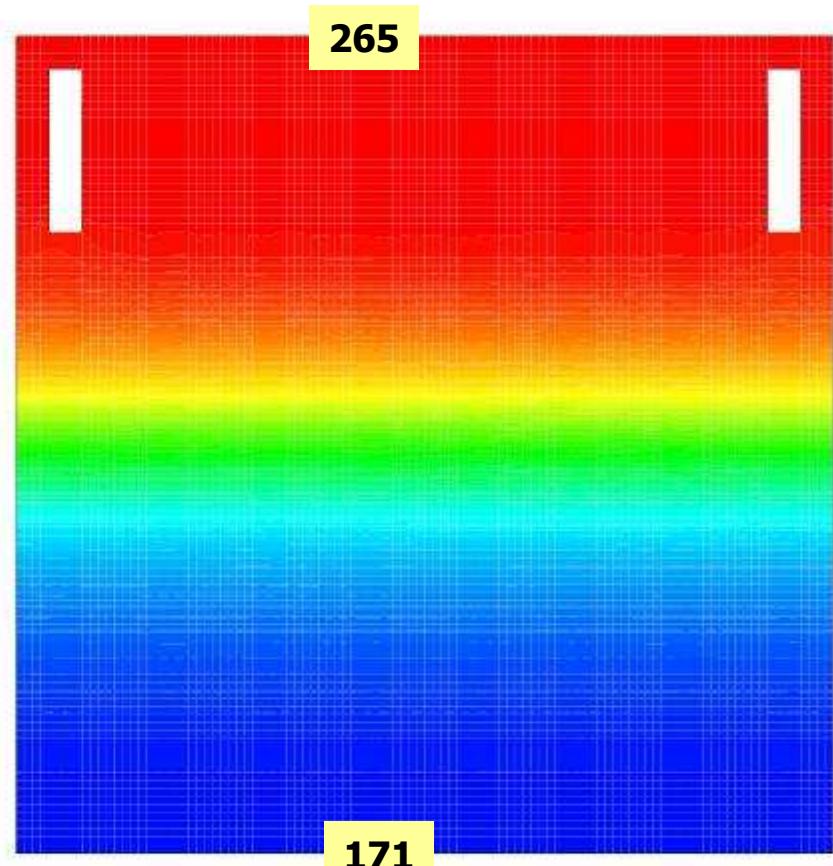
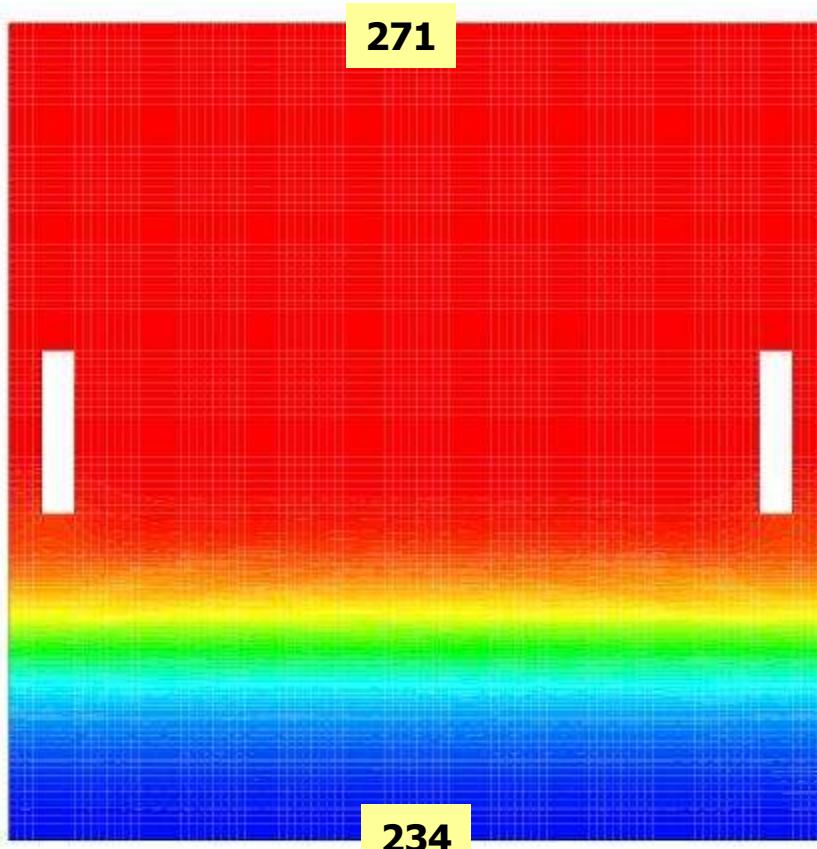
- No stratification only for the lower elevation (not shown, homogeneous dry hydrogen fraction of  $\approx 1.3\%$ )



## Temperature (C) at t=3000s

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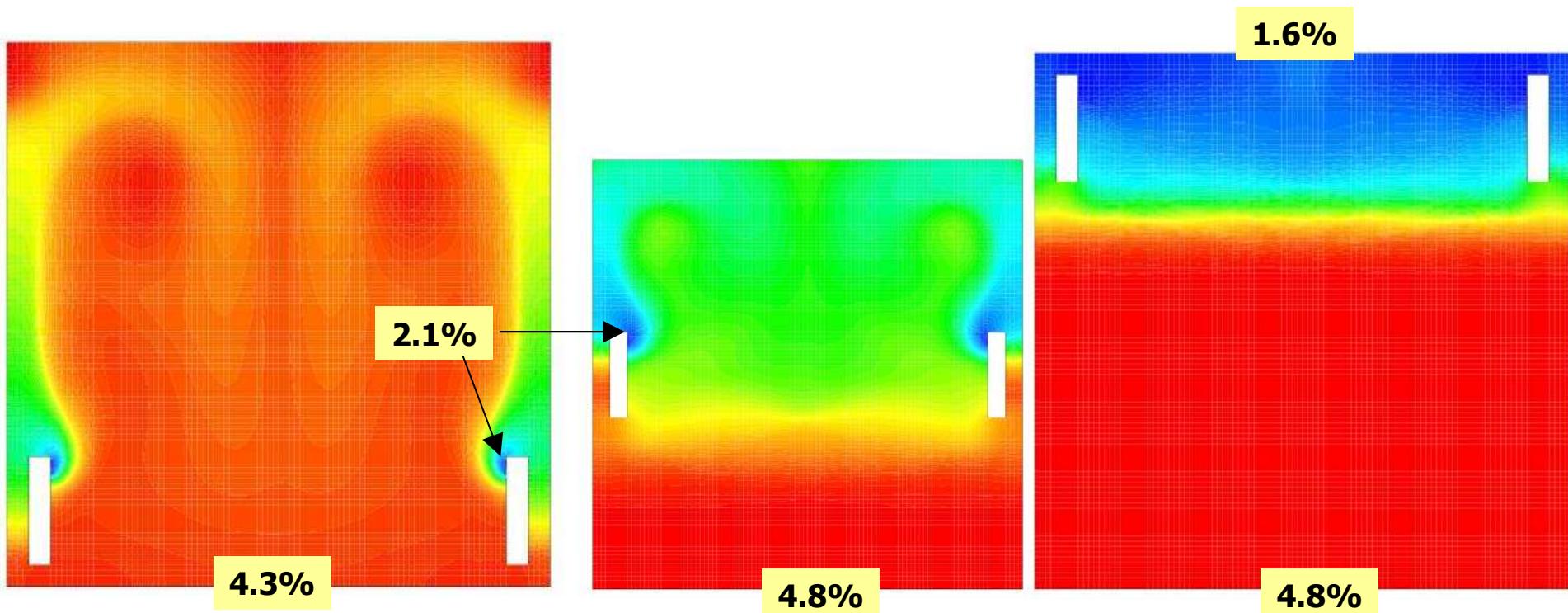
- No stratification only for the lower elevation (not shown, homogeneous temperature of 272C)



## Dry Xh2 at t=60s

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- Lower the PAR elevation is, larger the hydrogen mobilization is, longer burning and mixing processes are



# Conclusion

- Fast H<sub>2</sub> depletion rate but low mobilization below the PAR: an additional process is necessary to enhance mixing process and limit thermal and mass stratifications (wall heat and mass transfer, etc.)
- Code-to-code comparisons exhibit some differences:
  - For the transient phase, the flow pattern at the PAR outlet (plume or jet behaviour)
  - At the quasi steady-state, the floor layer diffusion

- Several interaction levels
  - PAR level (H<sub>2</sub> consumption rate, plates/flow interactions)
  - Nearfield level (PAR/atmosphere interactions)
  - Farfield level (H<sub>2</sub> distribution)
- Difficulties to deal with all space and time scales
  - Separate effect analysis is necessary
  - Farfield and nearfield connexions have to be understood
- Lack of experimental data
  - Lumped approaches of the KALI and H2PAR programs
  - REKO (FzJ) dedicated to H<sub>2</sub> consumption rate (plate interactions)
  - In project or in progress, larger scale programs dedicated to CFD code: PANDA (SETHII) and REKO 4 (FzJ) for example

# Acknowledgment

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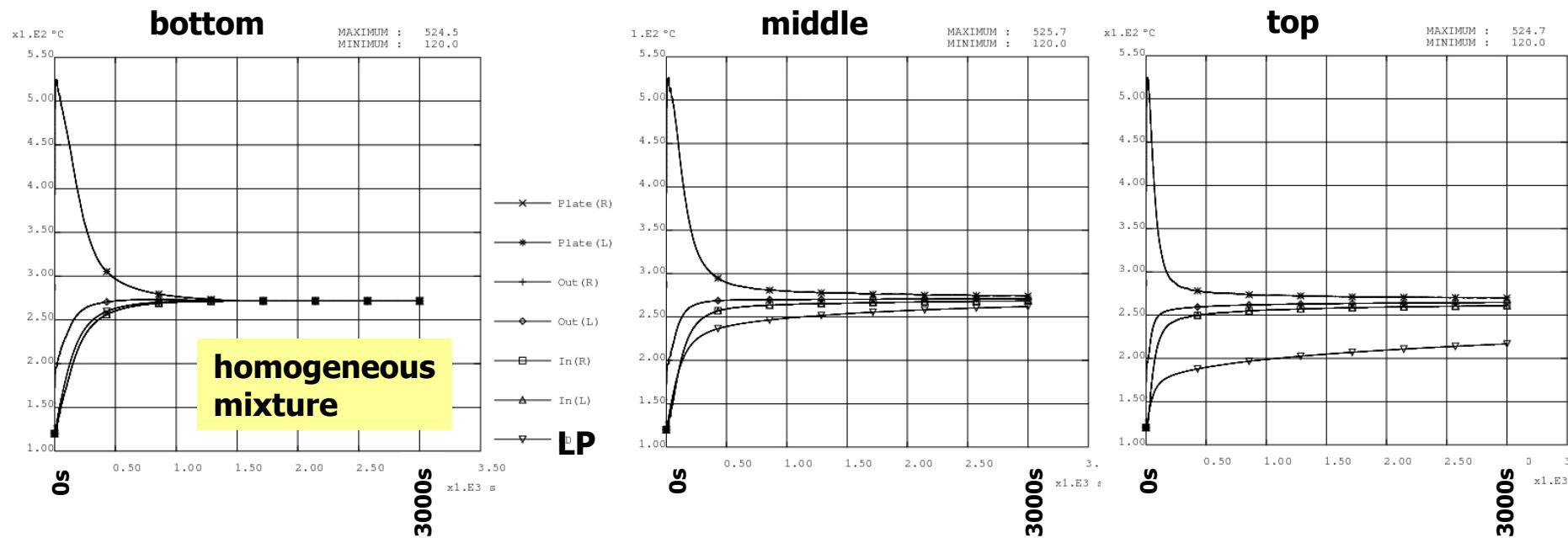


- Thanks to IRSN, AREVA TA and EU for their financial support
- Thanks for your attention

## PAR inlet/outlet and LP temperature evolution with time

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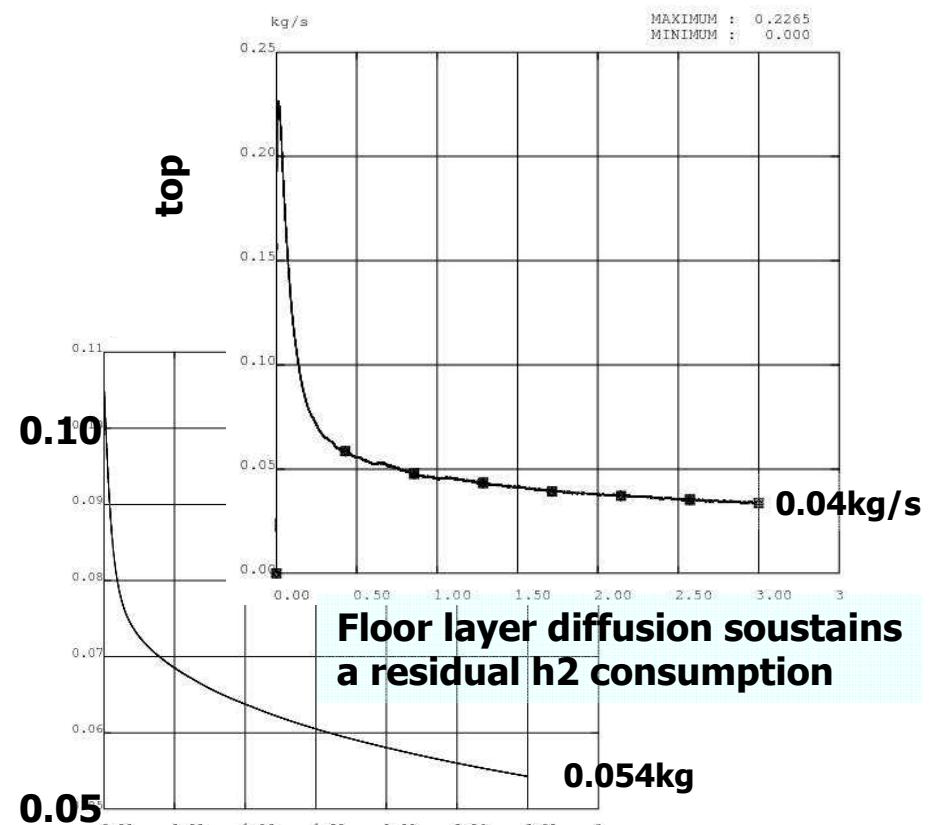
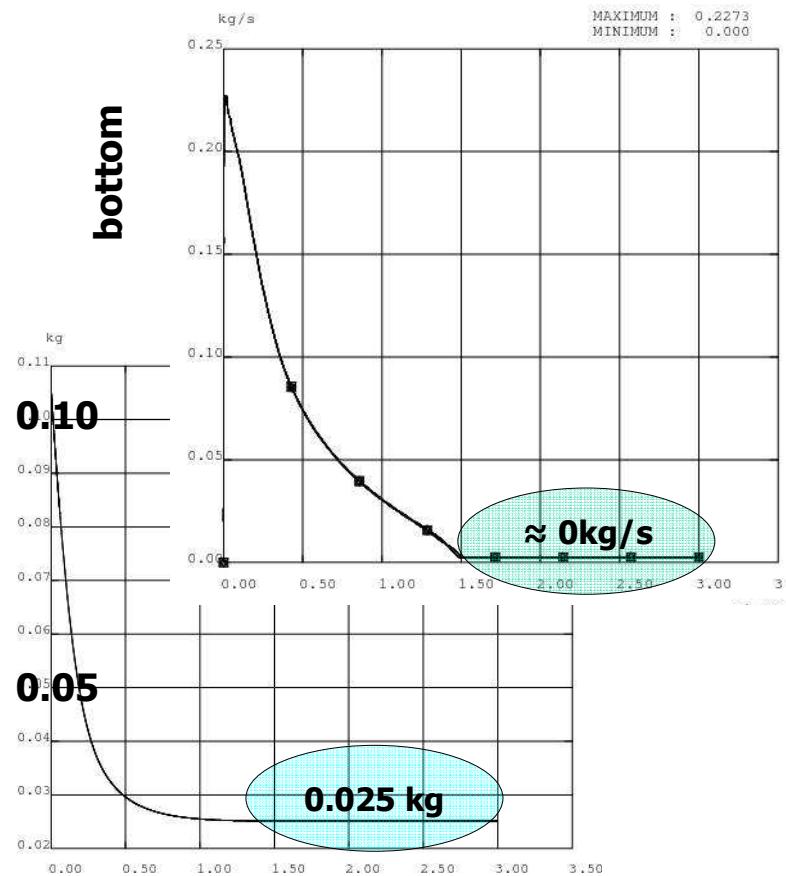
- No stratification only for the lower elevation (homogeneous,  $T=272^\circ\text{C}$ )
- Higher the PAR elevation is, larger the thermal stratification is
- More than 50°C of inlet/outlet temperature difference for the transient
- Decreasing plate temperature with time due to decreasing of H<sub>2</sub> consumption rate and mass flow rate through the PAR
- Left/right PAR symmetry is conserved



## PAR mass flow rate and H<sub>2</sub> mass evolution with time

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- At the lower elevation, the hydrogen molar fraction goes below the threshold value of 0.5%. Thus, the H<sub>2</sub> consumption rate goes to 0. So the mass flow rate because there is no more heat release.

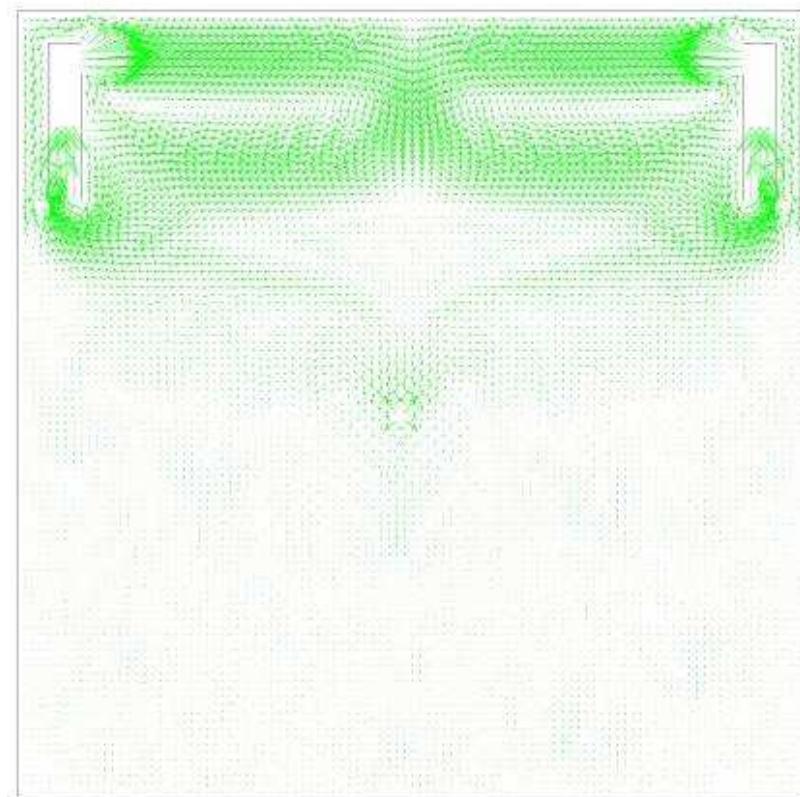
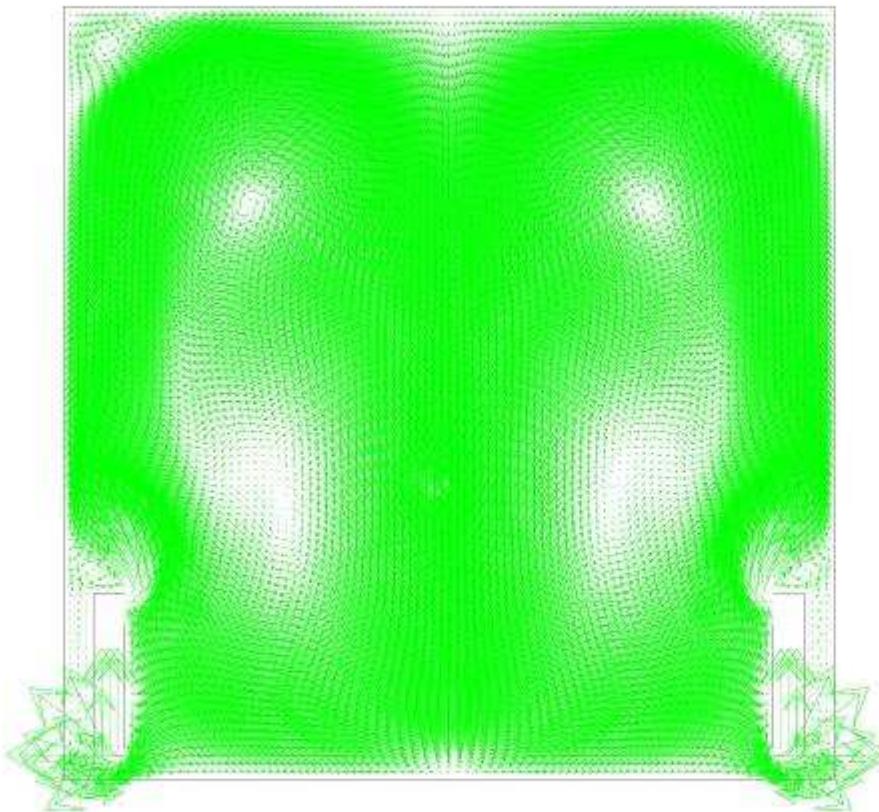


## Velocity at t=60s

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- Lower the PAR is, larger the hydrogen mobilization is
- 



## Dry Xh2 evolution along the left vertical line x=3w

cea

- No stratification only for the lower elevation (homogeneous T of 272°C)
- Higher the PAR elevation is, larger the mass stratification is

